

QUT Digital Repository:  
<http://eprints.qut.edu.au/>



Tellambura, Chintha and Jayalath, Dhammika (2001) PAR reduction of an OFDM signal using partial transmit sequences. In *Proceedings IEEE VTS 54th Vehicular Technology Conference, 2001 (VTC 2001 Fall)*. 2, pages pp. 465-469, Atlantic City, NJ, USA.

© Copyright 2001 IEEE

Personal use of this material is permitted. However, permission to reprint/republish this material for advertising or promotional purposes or for creating new collective works for resale or redistribution to servers or lists, or to reuse any copyrighted component of this work in other works must be obtained from the IEEE.

# PAR reduction of an OFDM signal using partial transmit sequences

C. Tellambura and A. D. S. Jayalath  
SCSSE, Faculty of Information Technology  
Monash University, Clayton Victoria 3168, Australia  
Email: chintha@dgs.monash.edu.au

**Abstract**—The peak-to-average power ratio (PAR) of an orthogonal frequency division multiplexing (OFDM) signal can be substantially larger than that of a single carrier system. Partial transmit sequence (PTS) combining can improve the PAR statistics of an OFDM signal. For PTS, the search complexity increases exponentially with the number of subblocks. Here, we present a new algorithm for computing the phase factors that achieves *better* performance than the exhaustive *binary* search approach. We also investigate the effects of non-linear amplifiers on the performance of the new algorithm, including the power spectral density and in-band distortion.

**Index terms** - OFDM, Peak-to-average power ratio

## I. INTRODUCTION

Orthogonal frequency division multiplexing (OFDM) has been proposed for both digital TV broadcasting and high speed wireless networks over multipath channels [1]. The principal drawback of OFDM is that the peak transmitted power can be substantially larger than the average power. Linear amplifiers that can handle the peak power are less efficient. Hard limiting of the transmitted signal generates intermodulation products that are capable of interfering with adjacent channels. Given these problems, following [2], which first described a block coding technique to reduce the signal peaks, many PAR issues have been studied in the literature (see [3–5] as examples among many others).

The PTS [6] approach is a distortionless technique based on combining signal subblocks which are phase-shifted by constant phase factors. The technique significantly reduces the PAR. Unfortunately, finding the optimal phase factors is a complex, non-linear optimization problem. Nevertheless, even with the phase factors discretized to 0 and  $\pi$ ,  $\text{PAR}_3$  can be reduced by more than 4 dB for a 256-subcarrier, quadrature phase shift keyed (QPSK) modulated OFDM system that is partitioned into 16 signal subblocks (throughout the paper we denote by  $\text{PAR}_n$  a value such that  $\Pr(\text{PAR} > \text{PAR}_n) = 10^{-n}$ ). If the phase factors are discretized to four levels, for 128 subcarriers and four signal subblocks,  $\text{PAR}_2$  is reduced by more than 3 dB. These impressive gains are realized by using what is known as an *optimal binary phase sequence* (OBPS), which was originally suggested in [6]. With this approach, the phase factors are restricted to 0 and  $\pi$  and hence an exhaustive search can be carried out over all combinations of permissible phase factors. A drawback to this approach is that the complexity of the OBPS search increases exponentially with the number of subblocks. In an effort to simplify the PTS method, a recent paper [4] has introduced new algorithms which per-

form *worse* than the OBPS solution but are much less complex. Note, at this point, that since the OBPS search uses binary quantized phase factors, it does not yield the global optimum solution for PTS.

The purpose of this paper to present a new algorithm that is able to compute best phase factors for PTS. This algorithm performs *better* than the OBPS solution. For a 256-subcarrier system,  $\text{PAR}_4$  can be reduced by approximately 5 dB using the new algorithm. Furthermore, the complexity of the new algorithm does not increase exponentially with the number of subblocks. We also investigate the effects of non-linear amplifiers on the performance of the new algorithm, including the power spectral density (PSD) and in-band distortion.

## II. PHASE FACTOR COMPUTATION FOR PTS

The complex envelope of the transmitted OFDM signal is represented by

$$s(t) = \frac{1}{\sqrt{N}} \sum_{n=0}^{N-1} X_n e^{j2\pi nt} \quad (1)$$

where  $j = \sqrt{-1}$  and  $X_n \in \{1, j, -1, -j\}$  (for simplicity, we consider QPSK modulation only). We shall write the input data block as a vector,  $\mathbf{X} = [X_0, \dots, X_{N-1}]^T$ . Most PAR-reduction techniques are concerned with reducing  $\max |s(t)|$ . However, since most systems employ discrete-time signals, the maximum amplitude of  $LN$  samples of  $s(t)$  is reduced instead, where  $L$  is the oversampling factor. The case  $L = 1$  is known as critical sampling or Nyquist rate sampling. The case  $L > 1$  corresponds to oversampling. Sampling can be implemented by a suitably zero-padded, inverse Fast Fourier transform (IFFT).

For the PTS approach, the input data vector  $\mathbf{X}$  is partitioned into disjoint subblocks, as  $\{\mathbf{X}_m | m = 1, 2, \dots, M\}$ , and these are combined to minimize the PAR. While several subblock partitioning schemes do exist, we assume the simplest scheme for which the subblocks consist of a contiguous set of subcarriers and are of equal size. Now, suppose that for  $m = 1, \dots, M$ ,  $\mathbf{A}_m = [A_{m1}, A_{m2}, \dots, A_{m, LN}]^T$  is the zero-padded IFFT of  $\mathbf{X}_m$ . These are the partial transmit sequences. The objective is thus to combine these with the aim of minimizing the PAR. The signal samples at the

output of the PTS combiner can be written as

$$\mathbf{S} = \begin{bmatrix} A_{11} & A_{21} & \dots & A_{M1} \\ A_{12} & A_{22} & \dots & A_{M2} \\ \dots & \dots & \dots & \dots \\ A_{1LN} & A_{2LN} & \dots & A_{MLN} \end{bmatrix} \begin{bmatrix} e^{j\phi_1} \\ e^{j\phi_2} \\ \vdots \\ e^{j\phi_M} \end{bmatrix} \quad (2)$$

where  $\mathbf{S} = [S_1(\Phi), \dots, S_{LN}(\Phi)]^T$  contains the optimized signal samples. We shall write the phase factors as a vector,  $\Phi = [\phi_1, \phi_2, \dots, \phi_M]^T$ . The phase factors  $\{\phi_k\}$  are chosen to minimize the peak of the signal samples  $|S_k(\Phi)|$ . So the minimum PAR is related to the problem

$$\begin{aligned} & \text{minimize} \quad \max_{0 < k \leq LN} |S_k(\Phi)| \\ & \text{subject to} \quad 0 \leq \phi_m < 2\pi, \quad m = 1, \dots, M. \end{aligned} \quad (3)$$

Suppose  $\hat{\phi}_m$  to be the global optimal solution to this problem. Unfortunately, there appears to be no simple way to obtain  $\hat{\phi}_m$  analytically. For coherent demodulation, it is necessary to send  $\hat{\phi}_m$  to the receiver as side information. When  $\hat{\phi}_m$  is a continuous value, an infinite number of bits will be required as side information. The solution to this problem is to limit  $\hat{\phi}_m$  to a level from a finite number of predetermined levels (quantization). For differential demodulation, it is not necessary to send  $\hat{\phi}_m$  to the receiver, but  $M - 1$  subcarriers at the subblock boundaries have to be set aside as reference subcarriers.

#### A. Suboptimal Exhaustive Search (SES) Algorithms

The phase factors are restricted to a finite set of values and hence (3) is approximated by the problem

$$\begin{aligned} & \text{minimize} \quad \max_{0 < k \leq LN} |S_k(\Phi)| \\ & \text{subject to} \quad \phi_m \in \left\{ \frac{2\pi l}{W} \mid l = 0, \dots, W - 1 \right\}. \end{aligned} \quad (4)$$

If the number of rotation angles  $W$  is “sufficiently” large, the solution of (4) will approach that of (3). Furthermore,  $\phi_1$  can be fixed without any performance loss. Now, there are only  $M - 1$  free variables to be optimized and hence  $W^{M-1}$  distinct phase vectors,  $\Phi_i$ , need to be tested. As such, (4) is solved using  $W^{M-1}$  iterations; the  $i$ -th iteration involves computing  $LN$  signal samples, each of which is denoted by  $S_k(\Phi_i)$ , using (2) and choosing the maximum  $|S_k(\Phi_i)|$  value. At the end of each iteration, the phase vector is retained if the current value of  $\max |S_k(\Phi_i)|$  is less than the previous maximum. The phase vector that is retained after all the iterations are completed will be an approximation to the global optimal solution of (3).

In most reported studies,  $W = 2$  and one is able to obtain the OBPS. In some cases, the use of more rotation angles ( $W > 2$ ) has been found to yield diminishing returns.

In SES, the computational load consists of  $M$  IFFTs,  $MLN$  complex multiplications per iteration, and  $LN$  operations of  $|\cdot|$ . If  $W = 2$  or 4, the multiplications can be replaced by additions. It might also be possible to use FFT algorithms that are suitable for handling data sets with a large number of zeros in order to reduce complexity. Such

issues are not pursued in this letter. As the computational cost of  $M$  IFFTs is fixed for any algorithm, for comparative purposes, we ignore that fixed cost component and define the measure of complexity as

$$N_c = W^{M-1} LN. \quad (5)$$

This measure indicates the total number of operations of  $|\cdot|$  and multiplications required. Given that its value increases exponentially with  $M$ , SES may not be feasible for  $M > 8$ .

#### B. New algorithm

The motivation for a new algorithm arises from the following observation. For given  $\Phi$ , we have the  $i$ -th row of (2) as

$$S_i(\Phi) = A_{1i}e^{j\phi_1} + A_{2i}e^{j\phi_2} + \dots + A_{Mi}e^{j\phi_M} \quad (6)$$

where  $A_{ri}$ ,  $r = 1, 2, \dots, M$ , are fixed complex numbers dependent only on the input data frame. What choice of  $\Phi$  will minimize the amplitude of this sum? If we sort  $|A_{ri}|$  as

$$|A_{r_1i}| > |A_{r_2i}| > \dots > |A_{r_Mi}|,$$

where  $\{r_1, \dots, r_M\}$  is a permutation of  $\{1, \dots, M\}$ , and choose

$$\phi_{r_l} = \begin{cases} -\angle A_{r_l i} & l = 1, 3, \dots \\ \pi - \angle A_{r_l i} & l = 2, 4, \dots \end{cases} \quad (7)$$

where  $\angle$  denotes the phase angle of a complex number, then the minimum amplitude sample is given by

$$S_i(\Phi) = |A_{r_1i}| - |A_{r_2i}| + |A_{r_3i}| - \dots \quad (8)$$

The phase selection (7) yields nearly always the maximum amount of amplitude cancellation for the  $i$ -th signal sample. As a result, it is very easy to find  $\Phi$  that will nearly always minimize the amplitude of a single signal sample. Let  $\hat{\Phi}_i$  be the solution (7) that nearly always minimizes  $|S_i|$ . Each  $\hat{\Phi}_i$  can be viewed as a reasonable - but not necessarily the optimal - solution for (3). Our next step is therefore to compute all  $LN$  such solutions and choose the one that minimizes the maximum signal samples.

Similar to the SES algorithms for (4), the new algorithm can be applied in  $LN$  iterations to obtain a solution for (3); the  $i$ -th iteration involves computing  $LN$  signal samples  $S_k(\hat{\Phi}_i)$  using (2) and choosing the maximum of  $|S_k(\hat{\Phi}_i)|$ . At the end of each iteration, the phase vector is retained if the current value of  $\max |S_k(\hat{\Phi}_i)|$  is less than the previous maximum. There are two main differences between the SES algorithms and the new algorithm. First, the number of iterations changes from  $W^{M-1}$  to  $LN$ . Second, the phase vectors are computed differently. The phase factors from (7) are not restricted to 0 and  $\pi$ , which is the case for SES with  $W = 2$ . Rather, they are continuous variables between 0 and  $2\pi$ .

As with (5), we define the measure of complexity as

$$N_c = LN \times LN. \quad (9)$$

The first  $LN$  denotes the number of iterations and the second denotes the number of operations per iterations. As

well, for  $W = 2$ , comparison of (5) and (9) reveals that the new algorithm is more complex than SES for small  $M$  but less complex for large  $M$  ( $> 8$ ).

### III. NONLINEAR TRANSMITTER CHARACTERISTICS

The OFDM signal is subject to various hardware nonlinearities in both the transmitter and receiver. These include signal clipping in the analog to digital (A/D) converter, signal clipping in the IFFT and FFT processors with a limited word length, amplitude modulation (AM)/AM and AM/phase modulation (PM) distortion in the radio frequency (RF) amplifiers. Such non-linearities not only affect the performance of an OFDM system, but also may affect the system performance of an adjacent channel. The out-of-band noise of OFDM signals increases due to nonlinear power amplifiers operating at different back-offs. The high PAR of OFDM requires high back-offs at the amplifiers. The non-linear characteristics of the soft limiter and solid state power amplifier are shown below [7, 8].

#### A. Soft limiter (SL)

Since the AM/PM component is zero the nonlinear characteristics of a SL can be written as

$$g(x) = \begin{cases} x & |x| \leq A, \\ Ae^{j\varphi} & |x| > A, \end{cases} \quad (10)$$

Where  $x$  is the input to the SL,  $A$  is the saturated output and  $\varphi$  is the phase angle of the input  $x$ . Although most physical components will not exhibit this piecewise linear behavior, the SL can be a good model if the nonlinear element is linearized by a suitable predistorter.

#### B. Solid-state power amplifiers (SSPA)

The input out relationship of many solid-state power amplifiers (SSPA) can be modeled as

$$F[\rho] = \frac{\rho}{[1 + (\frac{\rho}{A})^{2P}]^{\frac{1}{2P}}} \quad (11)$$

$$\Phi[\rho] = 0.$$

where  $\rho = |x|$  and the parameter  $P$  controls the smoothness of the transition from the linear region to the limiting or saturation region. When,  $P \rightarrow \infty$  the SSPA model approximates the SL characteristics. The back off (BO) at the non-linear device can be defined in terms of maximum power output  $A^2$  as

$$BO = 10 \log_{10} \left\{ \frac{A^2}{E\{|x|^2\}} \right\} \quad (12)$$

where  $E\{|x|^2\}$  is the average of the input power to the non-linear device. For PSD results, it is convenient to define the normalized bandwidth  $B_n = fT$ , where  $T$  is the OFDM symbol duration.

### IV. RESULTS

To justify the new algorithm vis-a-vis the SES approach, it is necessary to demonstrate two things. First, we must

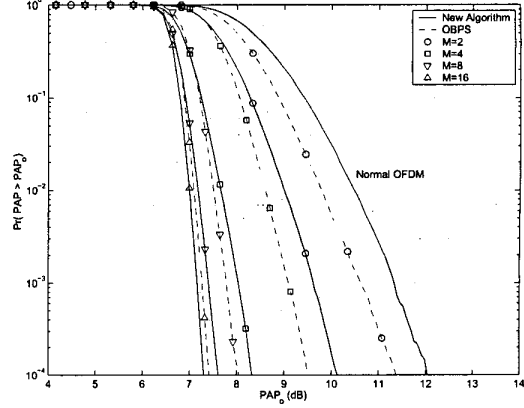


Fig. 1. Comparison of the new algorithm and the OBPS algorithm.

demonstrate that the PAR reduction achieved with the new algorithm is better and its complexity less than or similar to that of SES. Second, we must also demonstrate that, if the phase factors used in the new algorithm are quantized, the resulting performance loss will be small. This is particularly relevant if coherent demodulation is to be employed. These two issues are studied by simulation. In the results which follow,  $10^5$  OFDM signals are generated in each case. The transmitted signal is oversampled by a factor of 4 ( $L = 4$ ). All results are for 256-subcarrier and QPSK-modulated systems.

Fig. 1 compares the performance of the two algorithms as function of  $M$ , the number of subblocks. For  $M = 2, 4$ , the new algorithm performs more than 1 dB better than the OBPS solution. For  $M = 8$ , the performance gain is about 0.5 dB. For  $M = 16$ , both the algorithms perform nearly equally. However, in this case, the OBPS search requires  $2^{15}$  operations per iteration. As this would take up an enormous amount of computer time, the results for the  $M = 16$ , OBPS curve are shown for a limited, random search of the phase factor space. We performed only 500 trials and in [4] it was observed that 2000 trials would result in performance which was essentially equivalent to the OBPS. If the entire  $2^{15}$  combinations were tested at each iteration, we would expect the  $M = 16$ , OBPS curve to improve somewhat (i.e., it should be better than the new algorithm). Note that on the basis of (5) and (9), the OBPS search is 32 times more complex than the new algorithm for  $M = 16$ . We also tested the execution speed ratio for the two algorithms executed by Matlab on a 900 MHz Pentium machine. For  $M = 16$ , the OBPS algorithm was 20 times slower than the new algorithm. Thus, in this particular case and for a similar level of performance, the new algorithm is less complex. Based on this figure and other simulations not shown here, we can conclude the following: as  $M$  increases, the performance of both algorithms will converge while the complexity of the OBPS approach continues to increase exponentially.

Next, we consider quantization of the phase factors in the new algorithm to  $Q$  bits. That is, the phase factors (8) are rounded off to the nearest element in the set  $\{k\pi/2^{Q-1} | k =$

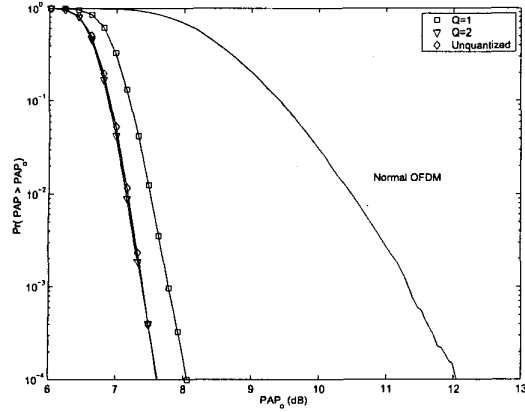


Fig. 2. The effect of quantization on the new algorithm, for  $M = 8$ .

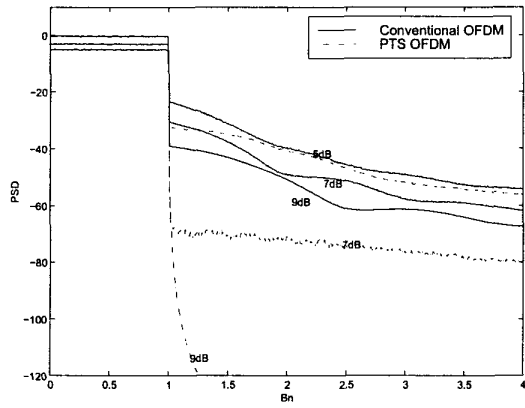


Fig. 3. Power spectral density of conventional OFDM and PTS-OFDM after soft limiting non-linear device.

$0, 1, \dots, 2^{Q-1}$ . The minimum overhead required to transmit all the phase factors to the receiver is then  $(M-1)Q$  bits. Fig. 2 shows results for  $Q = 1, 2$  and  $\infty$ . Even  $Q = 1$  achieves a performance level within 0.4 dB of the unquantized case ( $Q = \infty$ ). Performance degradation for the  $Q = 2$  case is negligible.

The conventional OFDM and PTS-OFDM signals are passed through SL and SAPA non-linear devices and the PSDs are estimated. Fig. 3 shows the PSD for a soft limiter with different back-off values. At 5 dB back off the out-of-band noise of the two signals is nearly the same. When the back off is increased to 7 dB, the out-of-band noise of PTS-OFDM is 20 dB below at  $B_n = 2$  to that of OFDM. This difference increases to 60 dB, when the back off is increased to 9 dB.

Somewhat similar performance is observed for a SSPA non-linear device, as depicted in Fig. 4. Again, no significant difference is observed for 5 dB back off, while out of band radiation is reduced by 10 dB and 50 dB at  $B_n = 2$  for 7 dB and 9 dB back offs. Therefore, it is evident that PTS with the new algorithm reduces the out-of-band noise of an OFDM signal significantly.

Fig.5 and 6 show the constellation diagrams of the re-

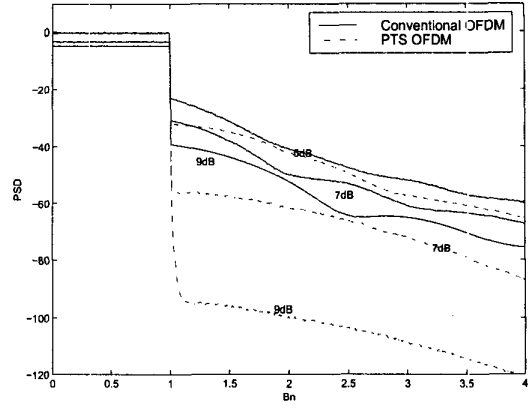


Fig. 4. Power spectral density of conventional OFDM and PTS-OFDM after SSPA non-linear device.

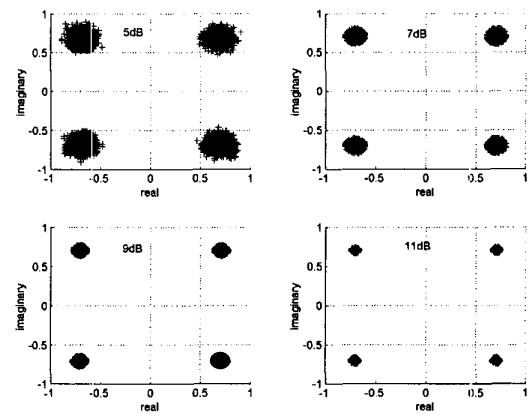


Fig. 5. Signal constellation at the receiver of conventional OFDM after SL non-linear device.

ceived signal of conventional OFDM and PTS-OFDM. A high level of in-band distortion occurs for conventional OFDM for a 5 dB back off. The severity of distortion reduces with the increasing back off. Even for an 11 dB back off some in-band signal distortion occurs. In contrast, in-band distortion occurs only for a 5 dB back off for PTS-OFDM. Clearly, the in-band signal distortion can be reduced significantly by using a PTS-OFDM.

## V. CONCLUSIONS

In conclusion, we observe that the PAR-reduction problem for OFDM has received a great deal of attention recently. In this paper, a new algorithm for computing a good set of phase factors for PTS combining has been developed. This algorithm performs better than the OBPS search for small  $M$ . As the number of subblocks increases, the performance difference between the two algorithms tends to zero, while the complexity of the OBPS solution increases exponentially. The effect of 2-bit quantization on the performance of the new algorithm is negligible. The out-of-band noise and in-band distortion of an OFDM signal can be significantly reduced by the use of PTS-OFDM with the new algorithm.

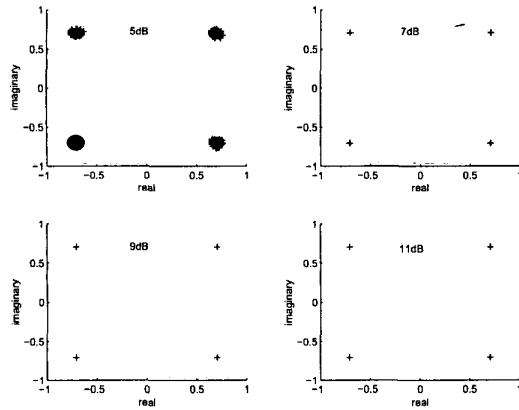


Fig. 6. Signal constellation at the receiver of PTS-OFDM ( $M = 16$ ) after SL non-linear device.

#### REFERENCES

- [1] J. A. C. Bingham, "Multicarrier modulation for data transmission: an idea whose time has come," *IEEE Commun. Magazine*, pp. 5–14, 1990.
- [2] A. E. Jones, T. A. Wilkinson and S. K. Barton, "Block coding scheme for reduction of peak to mean envelope power ratio of multicarrier transmission schemes," *Electron. Lett.*, vol. 30, pp. 2098–2099, 1994.
- [3] C. Tellambura, "Upper bound on the peak factor of N-multiple carriers," *Electron. Lett.*, vol. 33, pp. 1608–1609, Sept. 1997.
- [4] L. J. Cimini, Jr. and N. R. Sollenberger, "Peak-to-average power ratio reduction of an OFDM signal using partial transmit sequences," *IEEE Comm. Lett.*, vol. 4, pp. 86–88, Mar. 2000.
- [5] J. A. Davis and J. Jedwab, "Peak-to-mean power control in OFDM, Golay complementary sequences, and Reed-Muller codes," *IEEE Trans. Inform. Theory*, vol. 45, pp. 2397–2417, Nov. 1999.
- [6] S. H. Müller and J. B. Huber, "OFDM with reduced peak-to-average power ratio by optimum combination of partial transmit sequences," *Electron. Lett.*, vol. 33, pp. 368–369, Feb. 1997.
- [7] H. E. Rowe, "Memoryless nonlinearities with gaussian inputs: elementary results," *BELL Systems Tech. J.*, vol. 61, pp. 1519–1525, Sept. 1982.
- [8] G. Santella and F. Mazzenga, "A hybrid analytical simulation procedure for performance evaluation in m-qam-OFDM schemes in presence of nonlinear distortions," *IEEE trans. Vehicular Tech.*, vol. 47, pp. 142–151, Feb. 1998.